

# ANALYSIS AND DESIGN OF CONCRETE BUILDING

THE WESTINGHOUSE ELECTRIC COMPANY CORPORATE HEADQUARTERS

CRANBERRY, PA



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STRUCTURAL OPTION

AE SENIOR THESIS  
APRIL 14, 2009  
PENN STATE  
UNIVERSITY

# TOPIC OUTLINE

Background Information

Existing Conditions

Project Goals

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Design Implications

Lateral Loads

Schedule Comparison

Cost Analysis

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## THE WESTINGHOUSE ELECTRIC COMPANY CORPORATE HEADQUARTERS

- Building Background Information
  - Existing Building Conditions
  - Project Goals
  - Design Process
  - Design Implications and RAM Model
  - Lateral Loads and Considerations
- Schedule Comparison
- Cost Analysis Study
- Sustainable Architecture Study
- Recommendations
- Acknowledgements
- Questions

# BACKGROUND INFORMATION

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## THE WESTINGHOUSE ELECTRIC COMPANY CORPORATE HEADQUARTERS

- **Function:** Corporate Headquarters and Office Space
- **Project Size:** 434,800 sq. ft.
- **Stories:** 5 above grade, 1 below grade
- **Total Cost:** \$55,878,000
- **Construction:** February 2008 – May 2009
- **Building Location:** Cranberry, Pennsylvania

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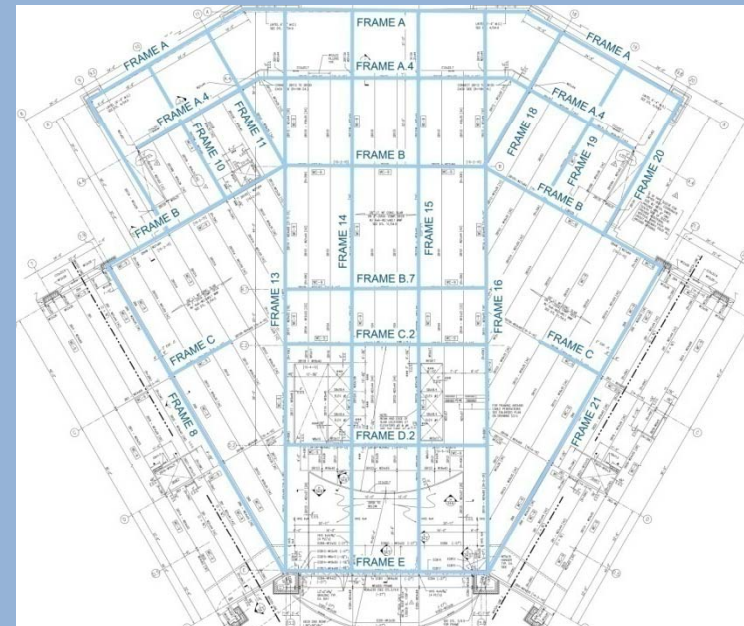
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## EXISTING STRUCTURAL STEEL FRAMING

- Steel framing
- Composite metal deck LWC topping
- Typical floor height 14'
- Foundation: Spread footings and caissons
- Moment connections at every column
- Typical bay size is 45'x24'



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- 434,800 SF BUILDING ONE
- BUILDINGS TWO AND THREE ON EACH SIDE TO START THE CAMPUS
- THE BUILDING IS EQUIPPED WITH AMENITIES SUCH AS:
  - CAFETERIA
  - GYM
  - LOCKER ROOMS
  - OFFICES
  - EXECUTIVE CONFERENCE ROOMS
- LEED CERTIFIED BUILDING GOAL



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- 83 ACRE SITE IN BUTLER COUNTY
- EASILY ACCESSIBLE FROM I-79, I-76, AND PA-228



Site Map From [www.google.com](http://www.google.com)

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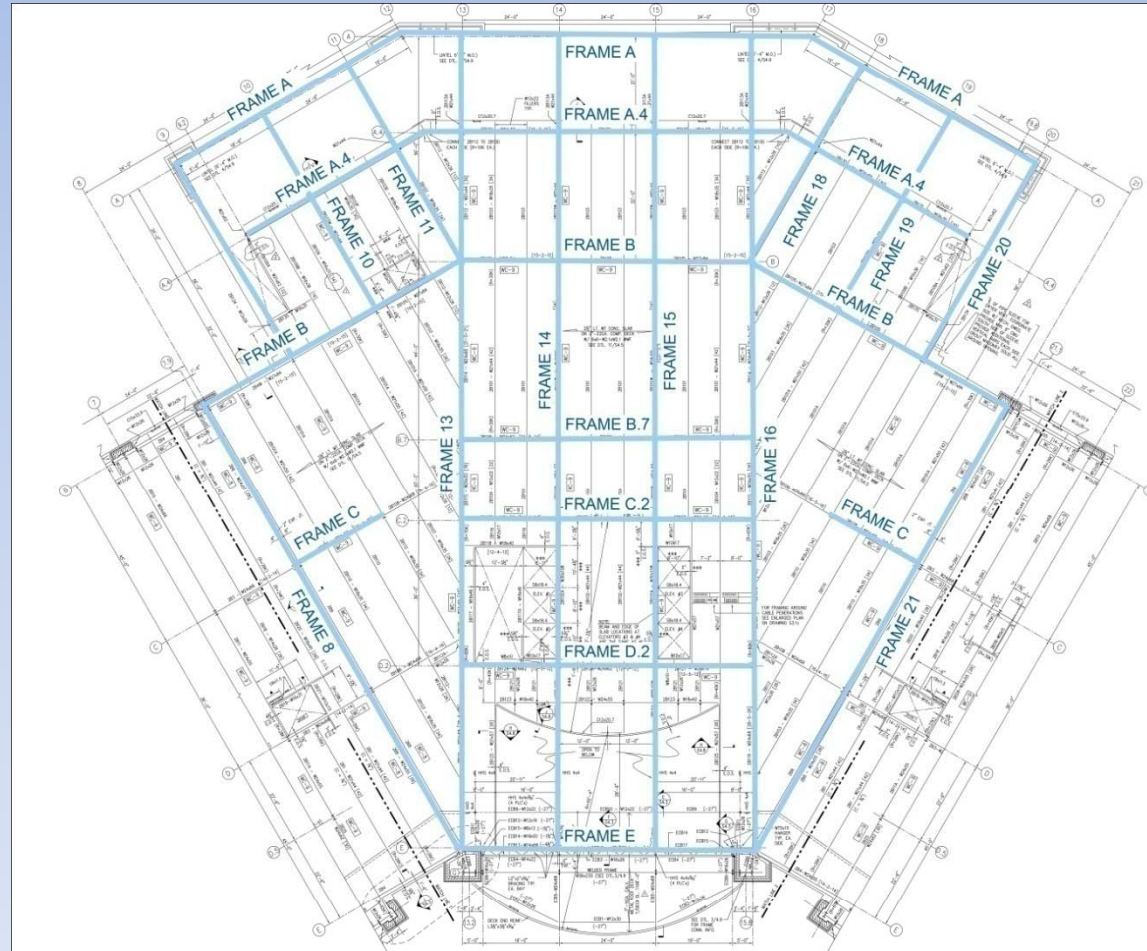
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# PROBLEM STATEMENT

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## Structural Depth

- The building has been shown to be effective with the existing system. However, the wind moment connections at every column could be more efficient.
- The typical bay size fits into the  $L_1/L_2 > 2$  requirement, making it ideal for a one-way slab.

## Construction Management Breadth

- Before a final decision can be made on the effectiveness of the new building structure, the systems must be compared for cost and construction time.

## Sustainable Architecture Breadth

- As a corporate headquarters, the building should make a statement.
- LEED certification is a requirement to the owner.
- A campus of this magnitude needs to be integrated into the environment.

# PROJECT GOALS

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## Structural Depth Goals

- Redesign the structural system using reinforced cast-in-place concrete and a one-way slab with beams floor system
- Implement the code effectively and efficiently
- Design a practical building

## Construction Management Breadth Study Goals

- Calculate a cost estimate for redesigned building
- Generate a schedule for redesigned building
- Effectively compare the new cost and schedule with Turner Construction Company's actual cost and schedule

## Sustainable Architecture Breadth Study Goals

- Incorporate the building into the environment
- Successfully implement a green roof
  - Detail, specify plants and materials, size drainage system pipes
- Determine number of LEED points possible for new design

# DESIGN PROCESS

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## Design Basis

- Dead load= weight of concrete + superimposed loads  
Live load= 70 PSF (50 Office and 20 Partition)
- Same building as the steel, only concrete
  - No beams, just girders and slab
- Additional load for green roof =100 PSF dead and patio live load= 100 PSF
- Hand design checked in RAM Structural System and rechecked with lateral by hand
- Foundations resized for new building

### Design Codes Used:

- IBC 2006
- ACI 318-08
- ASCE 7-05
- AISC Steel Construction Manual 13<sup>th</sup> Ed.

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## Concrete Design Considerations

- One-way slab  $L_1/L_2 > 2$
- Transverse reinforcement for shrinkage and temperature
- Moment transfer in concrete is different than in steel
- Foundation impact on spread footings and caissons
  - Resized for new dead load



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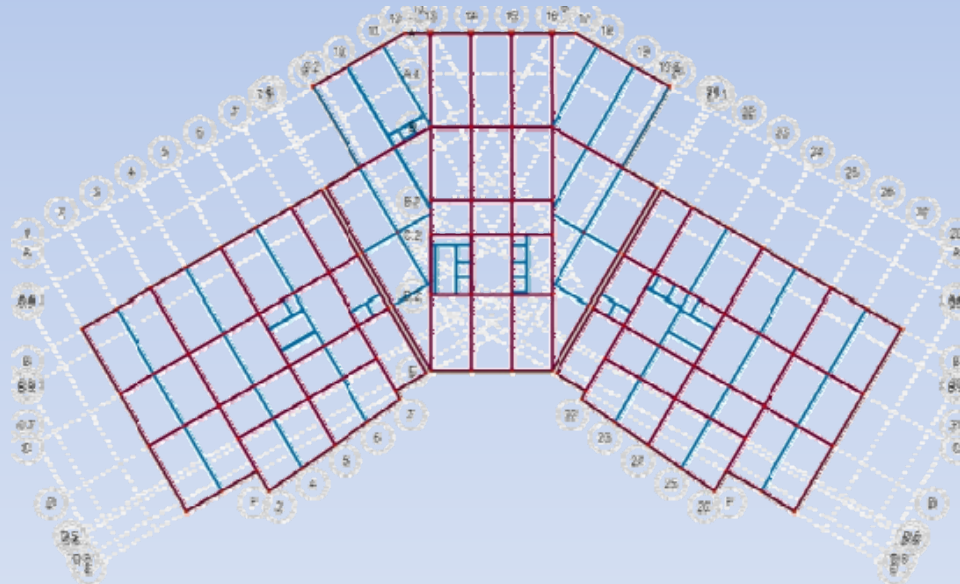
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## Design Process

- Determine superimposed loads from drawings and ASCE 7-05
- Perform a preliminary design of slabs, beams, and columns
- Determine location of CMRF's



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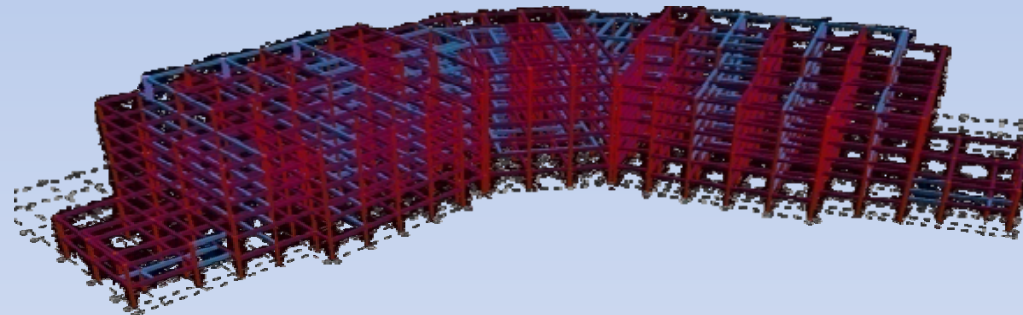
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## Design Process

- Determine superimposed loads from drawings and ASCE 7-05
- Perform a preliminary design of slabs, beams, and columns
- Determine location of CMRF's
- Create a RAM Structural System Model



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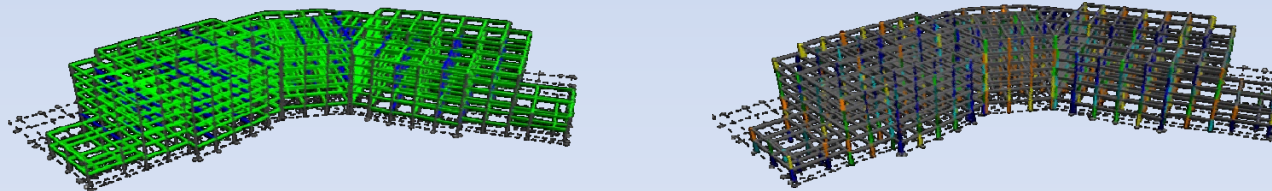
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## Design Process

- Determine superimposed loads from drawings and ASCE 7-05
- Perform a preliminary design of slabs, beams, and columns
- Determine location of CMRF's
- Create a RAM Structural System Model
- Compare the preliminary sizes to the RAM generated model sizes
- Hand calculation of lateral loads
- Update beam and column sizes for lateral loads in RAM model





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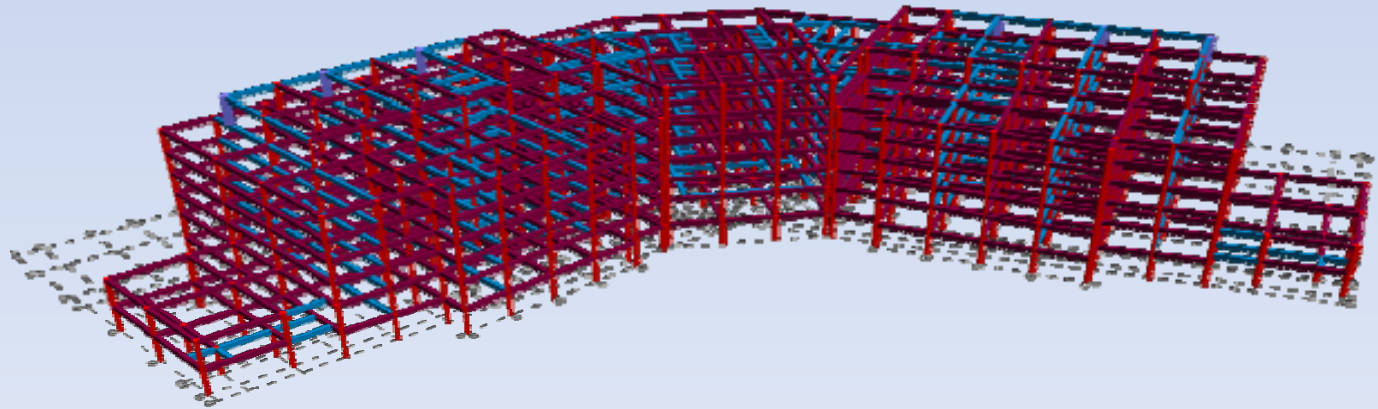
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## Design Process

- Determine superimposed loads from drawings and ASCE 7-05
- Perform a preliminary design of slabs, beams, and columns
- Determine location of CMRF's
- Create a RAM Structural System Model
- Compare the preliminary sizes to the RAM generated model sizes
- Hand calculation of lateral loads
- Update beam and column sizes for lateral loads in RAM model
- Spot check column sizes with PCA Column
- Spot check lateral beam by hand
- Update RAM model



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## Design Assumptions

- The ideal condition for the gravity members was assumed to be a simply supported beam
- The lateral members were assumed to be the ideal fixed-fixed connection to the columns
- The column connection to the foundation was assumed to be pinned
- The seismic response coefficient was assumed to be  $R=3.0$
- Model has ordinary moment frames in RAM Structural System
- Green roof and inclusive loads are present (separate analysis without performed for breadth)

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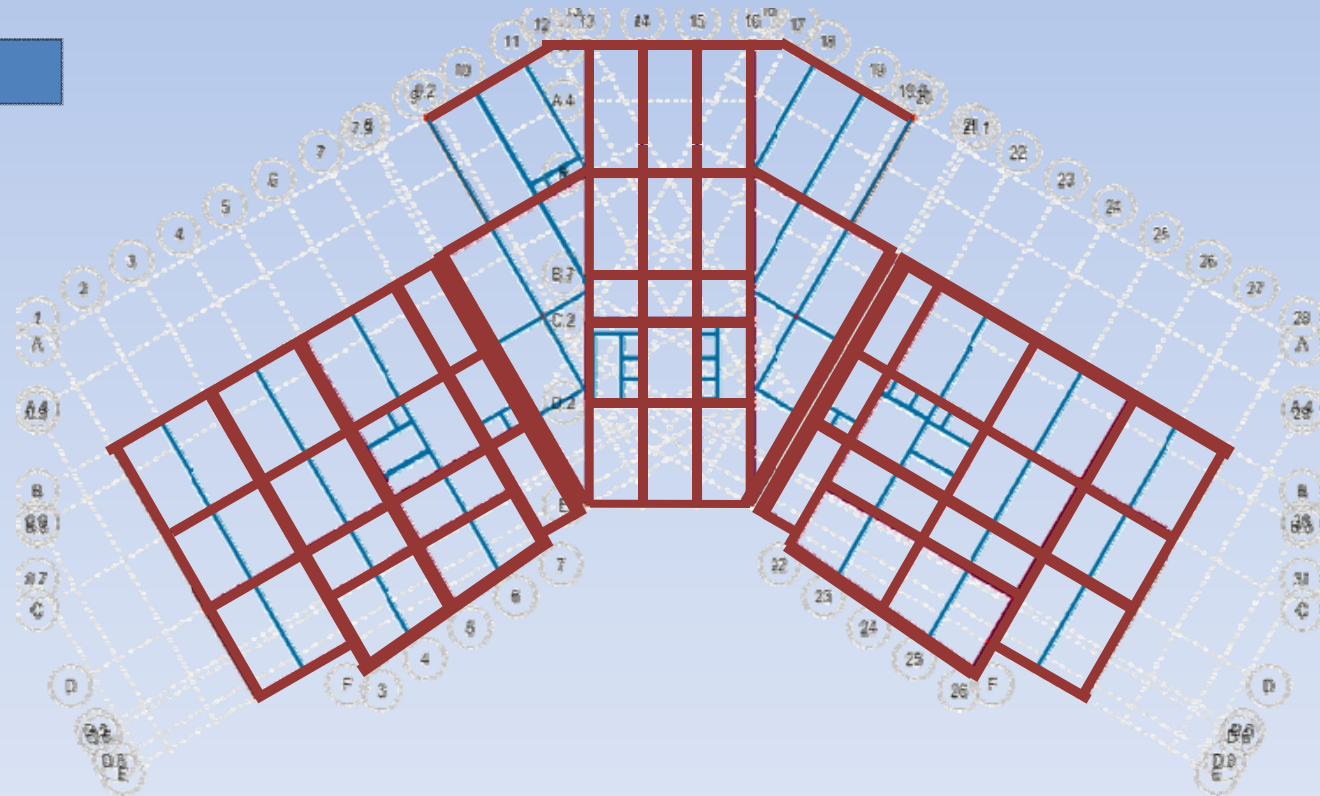
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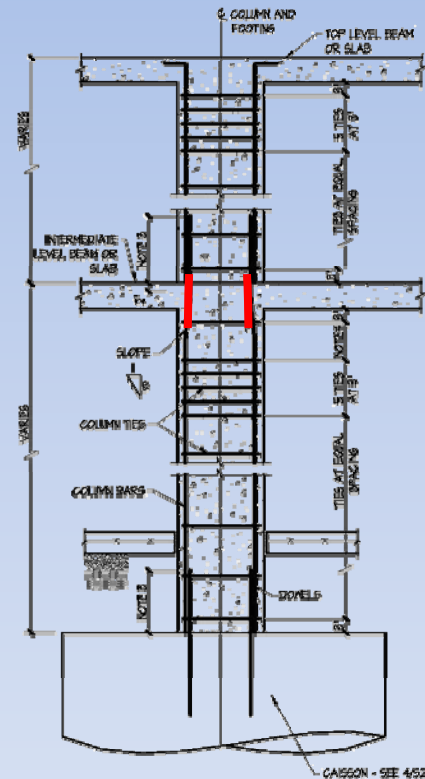
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## Design Process

### Concrete Moment Resisting Frame Detail



- NOTES:
- 1) SEE COLUMN SCHEDULE FOR DIMENSIONS AND REINFORCEMENT.
  - 2) SEE GENERAL NOTES FOR MINIMUM CONCRETE COVER TO PRIMARY REINFORCING.
  - 3) SEE 3/52-1 FOR SPLICE LENGTHS OF VERTICAL BARS.
  - 4) WHEN DIMENSION OF STIRRUP TO VERT BAR BEND EXCEEDS 6", PROVIDE ADDITIONAL TIE.

1 COLUMN BAR BENDING DETAIL NTS

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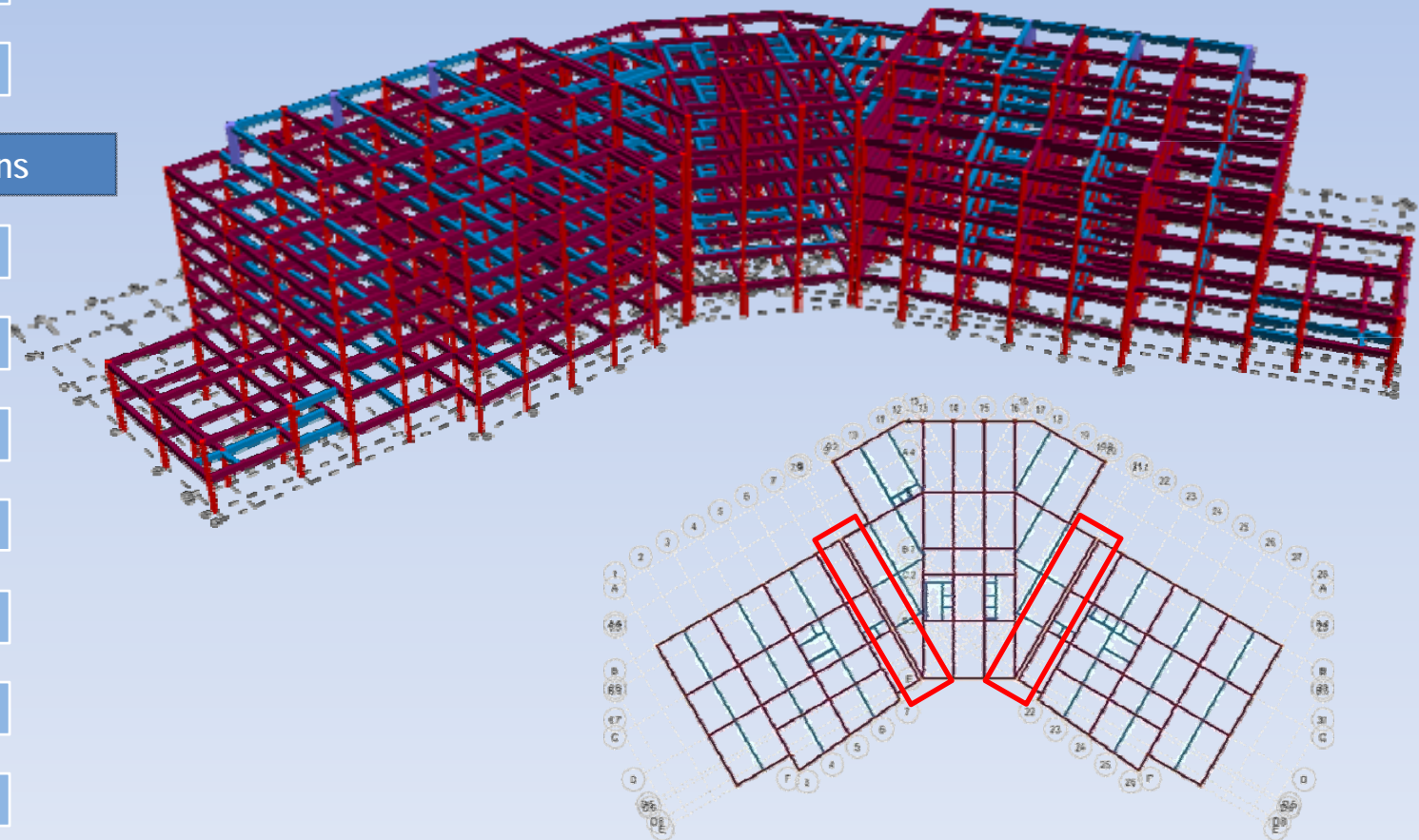
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## RAM STRUCTURAL SYSTEM MODEL

Whole building framing



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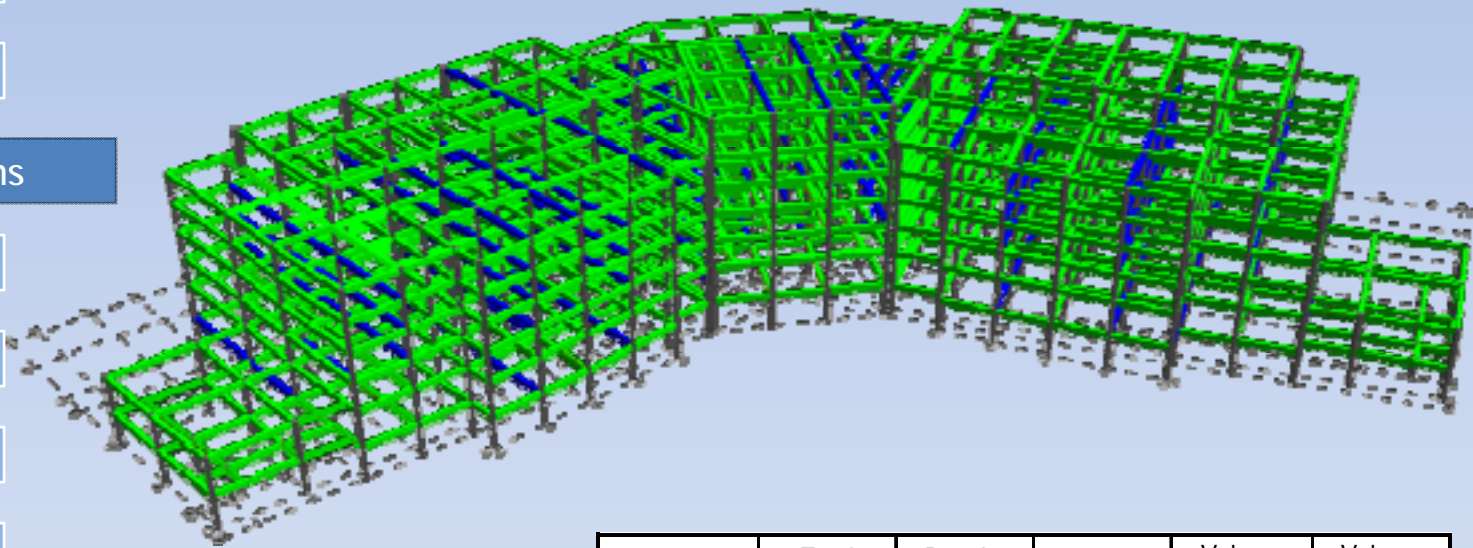
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## RAM STRUCTURAL SYSTEM MODEL

Whole building framing beams



Beam Size	Total Length (ft)	Density (PCF)	Weight (#)	Volume (ft <sup>3</sup> )	Volume (yd <sup>3</sup> )
24x34	32000.00	145	26293333	181333.33	6716.05
30x34	96	145	98600	680	25.19
34x34	223.87	145	260594.78	1797.2054	66.56
28x34	71.01	145	68067.78	469.43296	17.39
32x34	102.88	145	112711	777.32	28.79
Total Beam volume				185057.	6854.0

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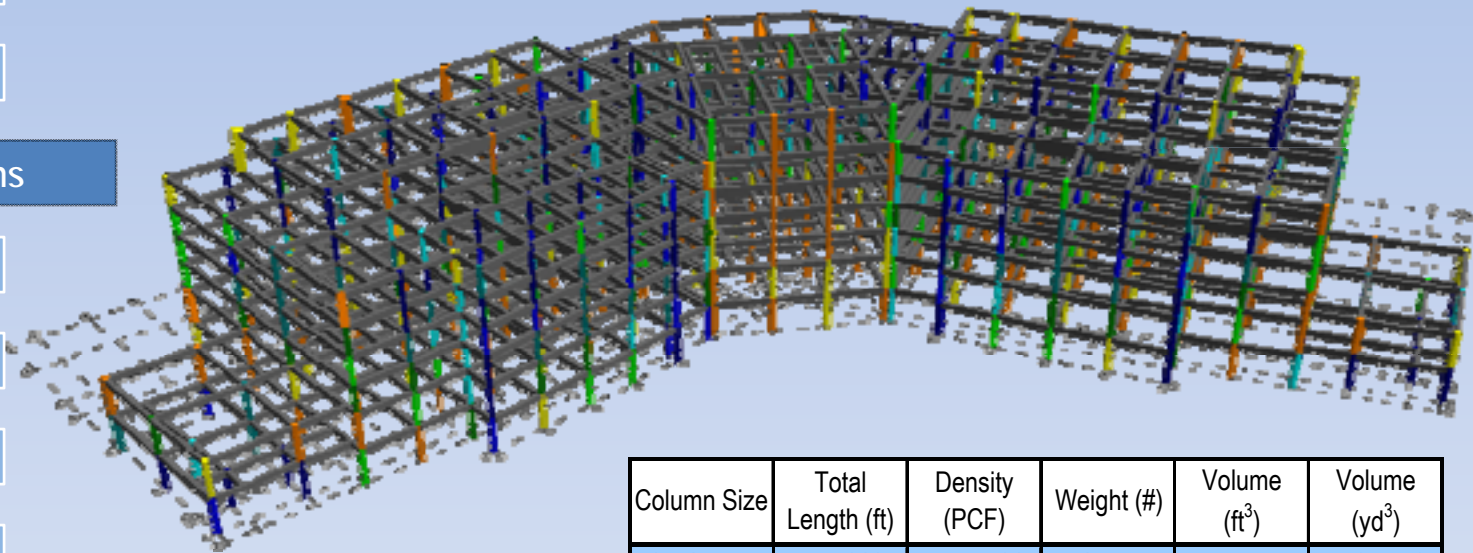
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## RAM STRUCTURAL SYSTEM MODEL

Whole building framing columns



Column Size	Total Length (ft)	Density (PCF)	Weight (#)	Volume (ft <sup>3</sup> )	Volume (yd <sup>3</sup> )
24x24	8141.5	145	4722070	32566	1206.15
28x28	622	145	360760	2488	92.15
30x30	986.5	145	572170	3946	146.15
32x32	72	145	41760	288	10.67
34x34	18	145	10440	72	2.67
36x36	182	145	105560	728	26.96
48x48	220	145	127600	880	32.59
Total Column Volume				40966	1517.33

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## FOUNDATION IMPLICATIONS

Old and New Foundation Sizes for spot checked columns

Size	Column	Type of Foundation	Size (ft)	Height (in)	Capacity (k)	Required (k)	Required Size	Required Height (in)	New Size (ft)	New Capacity (k)	Final Height (in)	RAM Size (ft)	RAM Height (in)
28	0.7-C	spread footing	5	18	200	384.844	6.936	18.273	7	392	22	8	24
24	1-B	spread footing	9.5	28	722	978.696	11.061	39.397	11.5	1058	44	11	36
24	1-C	spread footing	12	36	1152	1471.816	13.564	49.499	14	1568	54	13	42
24	1-D	spread footing	11	34	968	1606.032	14.169	51.518	14.5	1682	56	14	42
28	2-D	spread footing	12	36	1152	2179.108	16.504	56.044	17	2312	60	16	48
24	4-B	spread footing	10	32	800	1417.268	13.310	47.480	13.5	1458	52	13	42
30	1-E	caisson #48	5.5	146	712.749	957.832		146	7.00	1084.30	150		
28	6-B	spread footing	10	32	800	1454.464	13.484	42.858	13.5	1458	48	13	36
24	7.9-C	spread footing	13	40	1352	1342.364	12.954	45.460	13	1352	50	12	36
28	8-B	spread footing	11	34	968	922.328	10.737	33.426	11	968	38	11	30
24	8-C	spread footing	13	40	1352	1330.536	12.896	45.460	13	1352	50	12	36
48	13-A	spread footing	8	32	512	570.728	8.446	14.111	9	648	18	9	24
24	14-A.4	spread footing	8	32	512	418.416	7.232	25.211	8	512	30	7	18
24	15-B.7	spread footing	12	36	1152	1782.08	14.925	53.536	15	1800	58	14	48
28	16-E	caisson #53	4	306	376.991	1316.164		306	8.25	1399.22	310		



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## SEISMIC DESIGN LOADS

Floor	$w_x$ (k)	$h_x$ (ft)	$h_x^k$ (ft)	$w_x h_x^k$	$C_{vx}$	Story Force $F_x$ (k)	Story Shear $V_x$ (k)	Moment at Floor (ft-k)
Penthouse	6481.1	92.5	1115.41	7229044	0.179	293.33	0	27133.348
Roof	18245.1	74.5	797.56	14551503	0.361	590.46	293.33	43989.083
5	14162.0	60	570.24	8075727	0.200	327.69	883.79	19661.364
4	13922.9	46	377.75	5259370	0.130	213.41	1211.48	9816.8534
3	16960.3	32	215.24	3650482	0.091	148.13	1424.89	4740.0283
2	17785.3	18	88.23	1569200	0.039	63.67	1573.02	1146.1239
1	19178.2						1636.69	
Sum	106734.9	92.5	3164.42	40335326	1.000	1636.69	1636.69	106486.8

The seismic load for the redesigned concrete building is considerably larger than for the as-built steel building, which is to be expected since the new building is more massive.

Floor	$w_x$ (k)	$h_x$ (ft)	$h_x^k$ (ft)	$w_x h_x^k$	$C_{vx}$	Story Force $F_x$ (k)	Story Shear $V_x$ (k)	Moment at Floor (ft-k)
Penthouse	4213	92.5	1678.33	7070795	0.347	136.16	0	12594.449
Roof	4240.5	74.5	1176.85	4990465	0.245	96.10	136.16	7159.2331
5	4713.6	60	825.15	3889471	0.191	74.90	232.25	4493.7722
4	4726.5	46	533.66	2522321	0.124	48.57	307.15	2234.2278
3	4724.0	32	294.28	1390147	0.068	26.77	355.72	856.60376
2	4653.4	18	114.53	532940	0.026	10.26	382.49	184.72265
1	5444.4						392.75	
Sum	28502.4	74.5	2944.46	20396140	1.000	392.75	392.75	14928.56

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## WIND LOAD FOR THE REDESIGNED CONCRETE BUILDING

Level	Wind Design					
	Load (kips)		Shear (kips)		Moment (ft-k)	
	N-S	E-W	N-S	E-W	N-S	E-W
Pent	193.4	38.8	0	0	3481.3	698.2
Roof	151.5	30.2	193.4	38.8	2196.7	437.6
5	144.8	29.3	344.9	69.0	2026.7	410.7
4	138.0	28.1	489.7	98.3	1932.5	393.8
3	132.6	27.4	627.7	126.4	1856.3	384.1
2	140.2	31.0	760.3	153.9	2523.7	557.2
Total	900.5	184.8	900.5	184.8	10535.9	2183.4

## WIND LOAD FOR THE AS-BUILT STEEL BUILDING

Level	Wind Design					
	Load (kips)		Shear (kips)		Moment (ft-k)	
	N-S	E-W	N-S	E-W	N-S	E-W
Pent	196.5	39.6	0	0	3536.7	712.1
Roof	152.9	30.5	196.5	39.6	2217.2	442.4
5	146.0	29.7	349.4	70.1	2044.3	415.2
4	139.1	28.4	495.4	99.7	1948.0	397.7
3	133.5	27.7	634.6	128.1	1869.4	387.5
2	140.9	31.2	768.1	155.8	2536.6	562.0
Total	909.0	187.0	909.0	187.0	14152.2	2916.9



# SCHEDULE COMPARISON

## REDESIGNED BUILDING SCHEDULE

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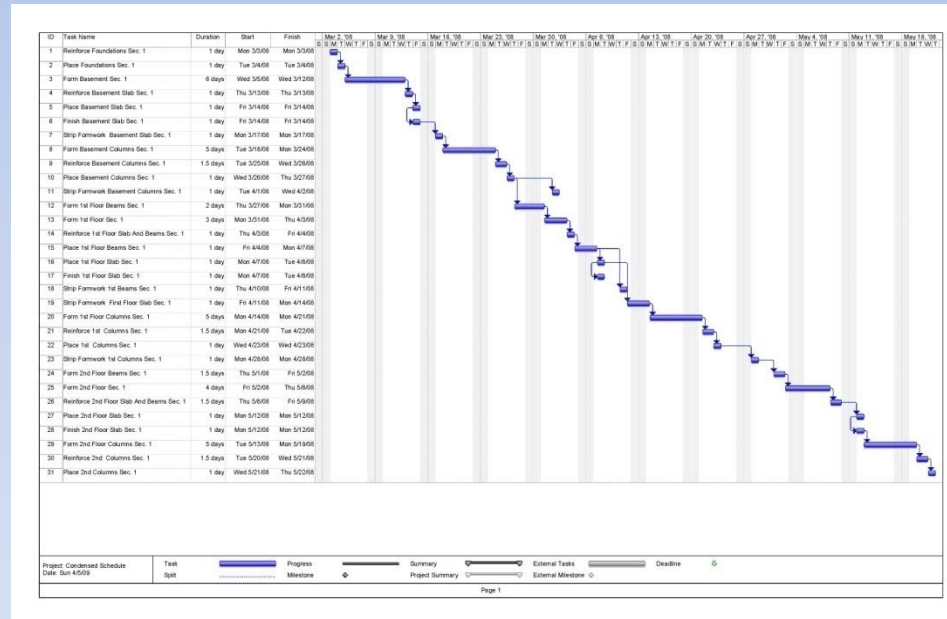
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- Start foundations on March 3<sup>rd</sup>, 2008
- Finish structure on December 9<sup>th</sup>, 2008
- Lead time for steel is insignificant -steel will be on site when foundations are finished



- Time difference because of sequencing, could potentially be sequenced differently if more crews were on site
- Turner pushed ahead with the schedule finishing before their estimated date effectively

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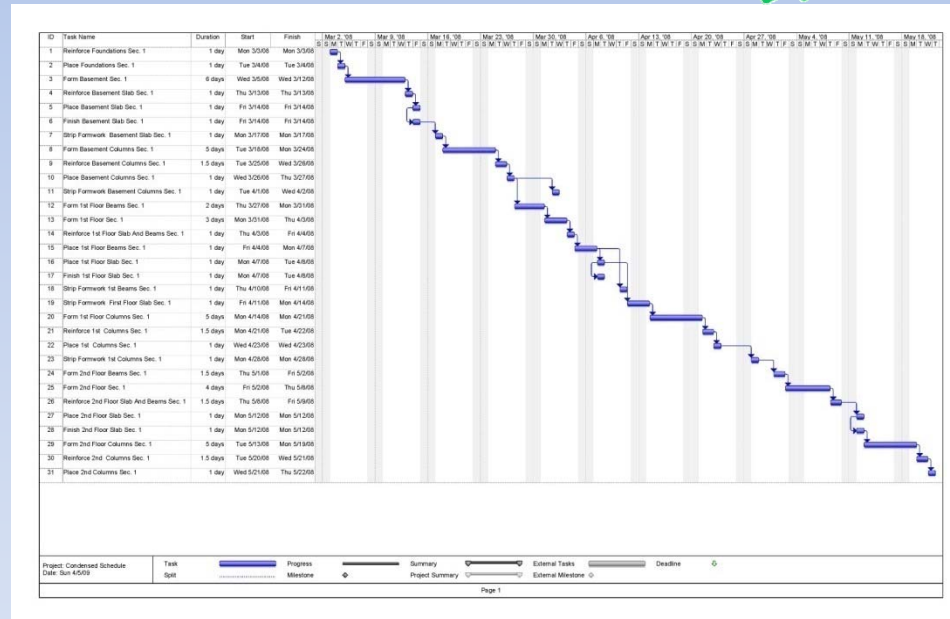
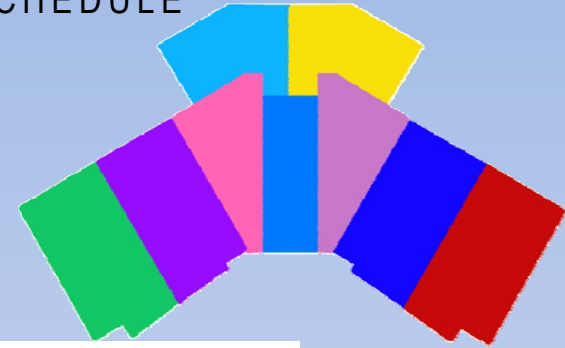
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## REDESIGNED BUILDING SCHEDULE



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# COST ANALYSIS STUDY

## REDESIGNED BUILDING ESTIMATE

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Detailed Cost Analysis of the Structure-No Green Roof									
Level	Description	Amount	Material Price	Material Cost	Labor Price	Labor Cost	Equipment Price	Equipment Cost	Total Cost
Reinforcement	Foundation	58 Ton	\$935.00	\$54,230	\$430.00	\$24,940	\$30.35	\$1,760	\$80,930
	Columns	156Ton	\$935.00	\$147,263	\$430.00	\$430.00	\$30.35	\$4,780	\$152,473
	Beam/Slabs	504 Ton	\$935.00	\$470,642	\$430.00	\$216,445	\$30.35	\$15,277	\$702,363
	<b>SUB-TOTAL</b>	<b>719</b>	<b>\$935.00</b>	<b>\$672,134</b>	<b>\$430.00</b>	<b>\$241,815</b>	<b>\$30.35</b>	<b>\$21,817</b>	<b>\$935,766</b>
Cast in Place Concrete	Foundations	6100 CY	\$109.00	\$664,900	\$14.90	\$90,890	\$5.55	\$33,855	\$789,645
	Columns	1443 CY	\$109.00	\$157,189	\$34.00	\$49,031	\$16.95	\$24,444	\$230,664
	Slabs	14192 CY	\$109.00	\$1,546,928	\$18.20	\$258,294	\$9.15	\$129,857	\$1,935,079
	Beams	6477 CY	\$109.00	\$706,026	\$26.50	\$171,648	\$1,320.00	\$8,550,036	\$9,427,710
	<b>SUB-TOTAL</b>	<b>28211</b>	<b>\$109.00</b>	<b>\$3,075,043</b>	<b>\$20.20</b>	<b>\$569,864</b>	<b>\$1,352</b>	<b>\$8,738,191</b>	<b>\$12,383,098</b>
Location Factor: 98.9%	<b>Total Structure Estimate:</b>			<b>\$13,173,000</b>			<b>Total Labor Cost:</b>		<b>\$812,000</b>
	<b>Total Material Cost:</b>			<b>\$3,748,000</b>			<b>Total Equipment Cost:</b>		<b>\$8,761,000</b>

## TURNER CONSTRUCTION COMPANY

Turner Construction Company Budgets	
Deep foundations (caissons)	\$215,000
Concrete (Spread ftgs, slabs)	\$5,199,000
Structural Steel	\$7,892,000
<b>Total Structure</b>	<b>\$13,306,000</b>
Whole Building	\$55,878,000

- \$30.60/SF vs. \$30.90/SF
- R.S. Means is not as accurate as real estimates
- Turner had contractors actually bid

# SUSTAINABLE ARCHITECTURE STUDY

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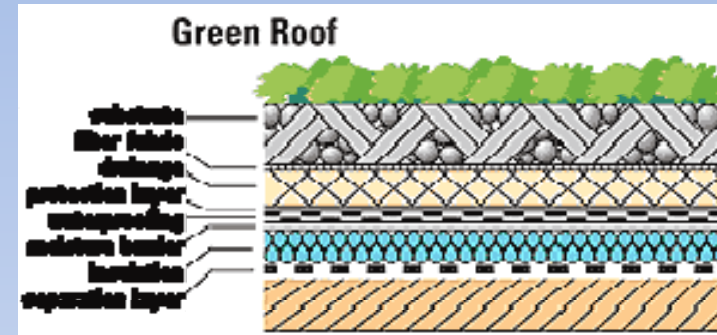
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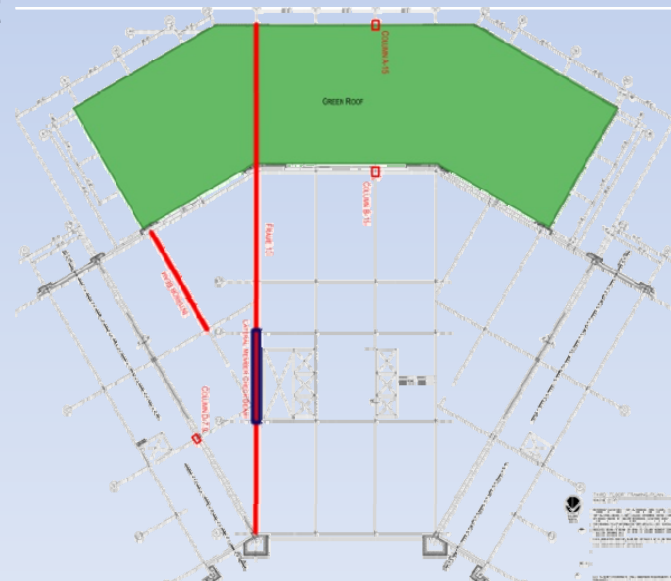
Questions

## THE WESTINGHOUSE ELECTRIC COMPANY CORPORATE HEADQUARTERS

- Functions and benefits
  - Patio
  - Meeting area
  - Lunch area
  - Storm water collector
  - Reduces heat island effect



[www.deq.state.mi.us/documents/deq-ess-p2-p2week-greenroofresources.doc](http://www.deq.state.mi.us/documents/deq-ess-p2-p2week-greenroofresources.doc)



# SUSTAINABLE ARCHITECTURE STUDY

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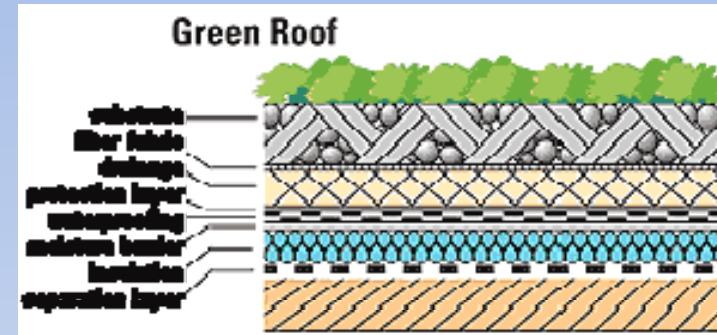
Recommendations

Acknowledgements

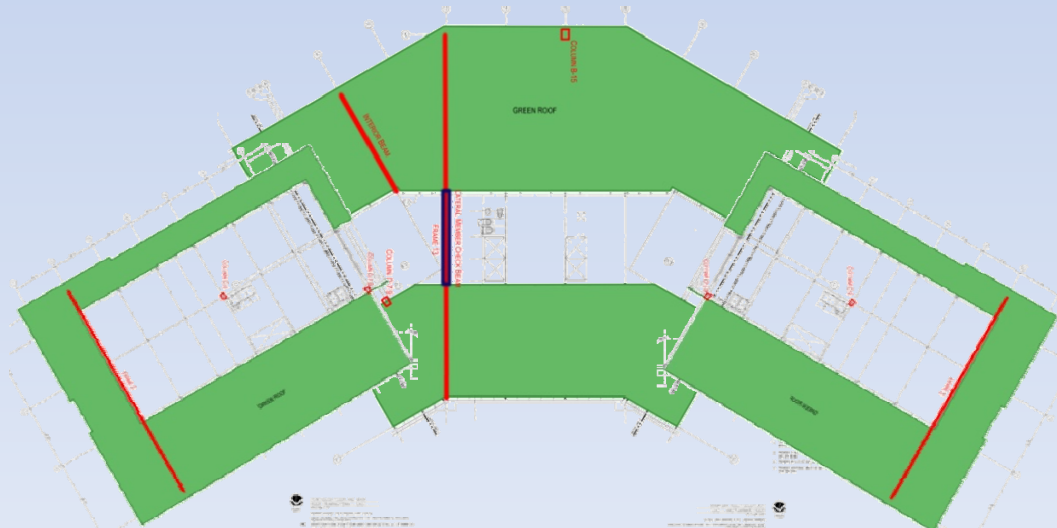
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## THE WESTINGHOUSE ELECTRIC COMPANY CORPORATE HEADQUARTERS

- Functions and benefits
  - Patio
  - Meeting area
  - Lunch area
  - Storm water collector
  - Reduces heat island effect



[www.deq.state.mi.us/documents/deq-ess-p2-p2week-greenroofresources.doc](http://www.deq.state.mi.us/documents/deq-ess-p2-p2week-greenroofresources.doc)





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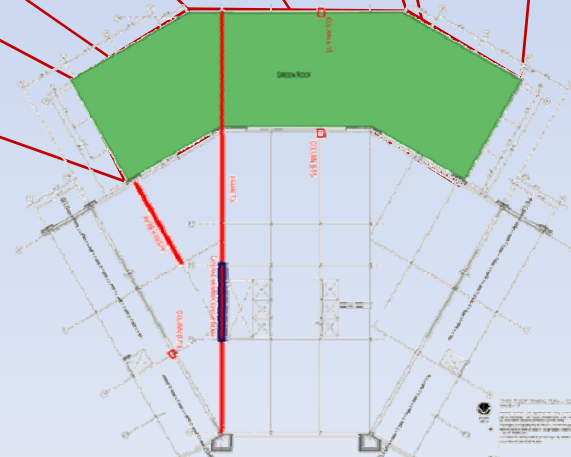
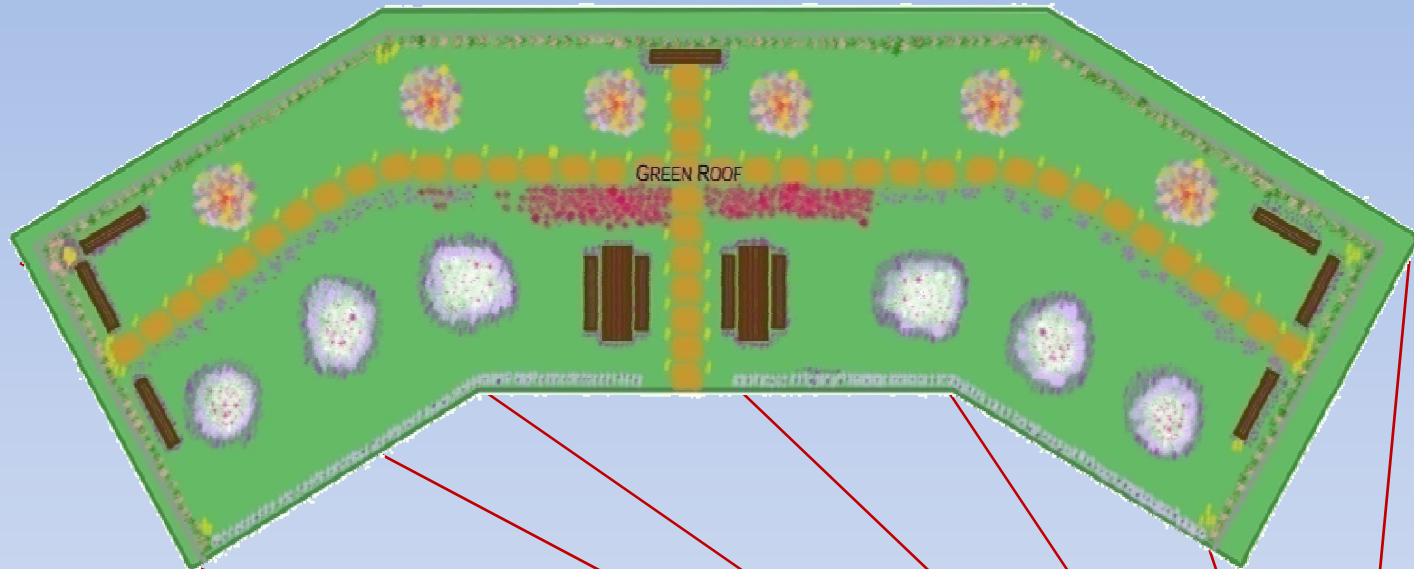
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Plant Layout on accessible roof on 3<sup>rd</sup> floor



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- No green roof structure costs \$13,173,000 or \$30.60/SF
- With green roof, structure costs \$1,159,000 or \$2.68/SF more
- Beam and columns needed to be resized, the slab was checked and found to be adequate
- Green roof adds 100 PSF dead and 100 PSF live load to the accessible portion

Detailed Cost Analysis of the Structure									
Level	Description	Amount	Material Price	Material Cost	Labor Price	Labor Cost	Equipment Price	Equipment Cost	Total Cost
Reinforcement	Foundation	58 Ton	\$935.00	\$54,230	\$430.00	\$24,940	\$30.35	\$1,760	\$80,930
	Columns	175 Ton	\$935.00	\$163,625	\$430.00	\$430.00	\$30.35	\$5,311	\$169,366
	Beam/Slabs	572 Ton	\$935.00	\$534,820	\$430.00	\$245,960	\$30.35	\$17,360	\$798,140
	<b>SUB-TOTAL</b>	<b>805</b>	<b>\$935.00</b>	<b>\$752,675</b>	<b>\$430.00</b>	<b>\$346,150.00</b>	<b>\$30.35</b>	<b>\$24,432</b>	<b>\$1,123,257</b>
Cast in Place Concrete	Foundations	6100 CY	\$109.00	\$664,900	\$14.90	\$90,890	\$5.55	\$33,855	\$789,645
	Columns	1518 CY	\$109.00	\$165,462	\$34.00	\$51,612	\$16.95	\$25,730	\$242,804
	Slabs	14192 CY	\$109.00	\$1,546,928	\$18.20	\$258,294	\$9.15	\$129,857	\$1,935,079
	Beams	7197 CY	\$109.00	\$784,473	\$26.50	\$190,721	\$1,320.00	\$9,500,040	\$10,475,234
	<b>SUB-TOTAL</b>	<b>29007</b>	<b>\$109.00</b>	<b>\$3,161,763</b>	<b>\$23.40</b>	<b>\$271,330</b>	<b>\$1,352</b>	<b>\$9,689,482</b>	<b>\$13,122,575</b>
Location Factor: 98.9%	<b>Total Structure Estimate:</b>			<b>\$14,332,000</b>			<b>Total Labor Cost:</b>		<b>\$863,000</b>
	<b>Total Material Cost:</b>			<b>\$3,915,000</b>			<b>Total Equipment Cost:</b>		<b>\$9,714,000</b>

- An additional week is needed to erect the green roof building than without it

# RECOMMENDATIONS

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- The building was successfully redesigned and the code was correctly implemented
- It is possible to have a reinforced concrete building
- Based on cost and schedule, this system is not recommended
  - \$30.90/SF vs. \$30.60/SF
  - March-October vs. March-December
- The addition of a green roof however, is recommended.
  - If the building were in concrete the green roof structural cost would be \$2.68/SF of building or \$20.24/SF of green roof
  - One additional week construction for the additional structure

# ACKNOWLEDGEMENTS

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I would like to thank:

- Turner Construction Company
  - Bob Hennessey
- LLI Engineering
- Westinghouse Electric Company
- Wells Real Estate Funds
- Penn State University
  - Dr. Hanagan
  - Prof. Parfitt
  - Prof Holland
  - And the rest of the AE faculty and staff
- Family and friends

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# QUESTIONS



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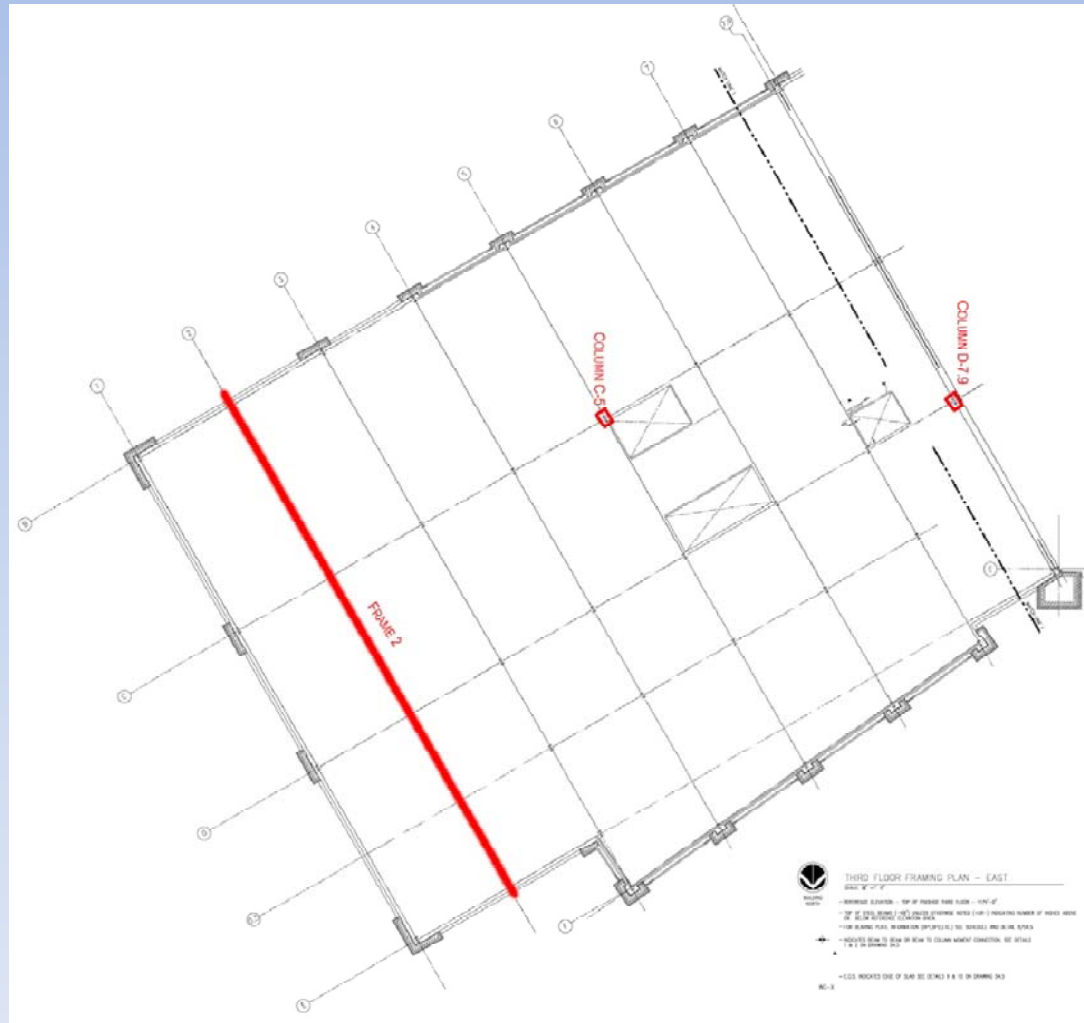
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## THIRD FLOOR EAST





# FLOOR PLANS

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## ROOF EAST





# FLOOR PLANS

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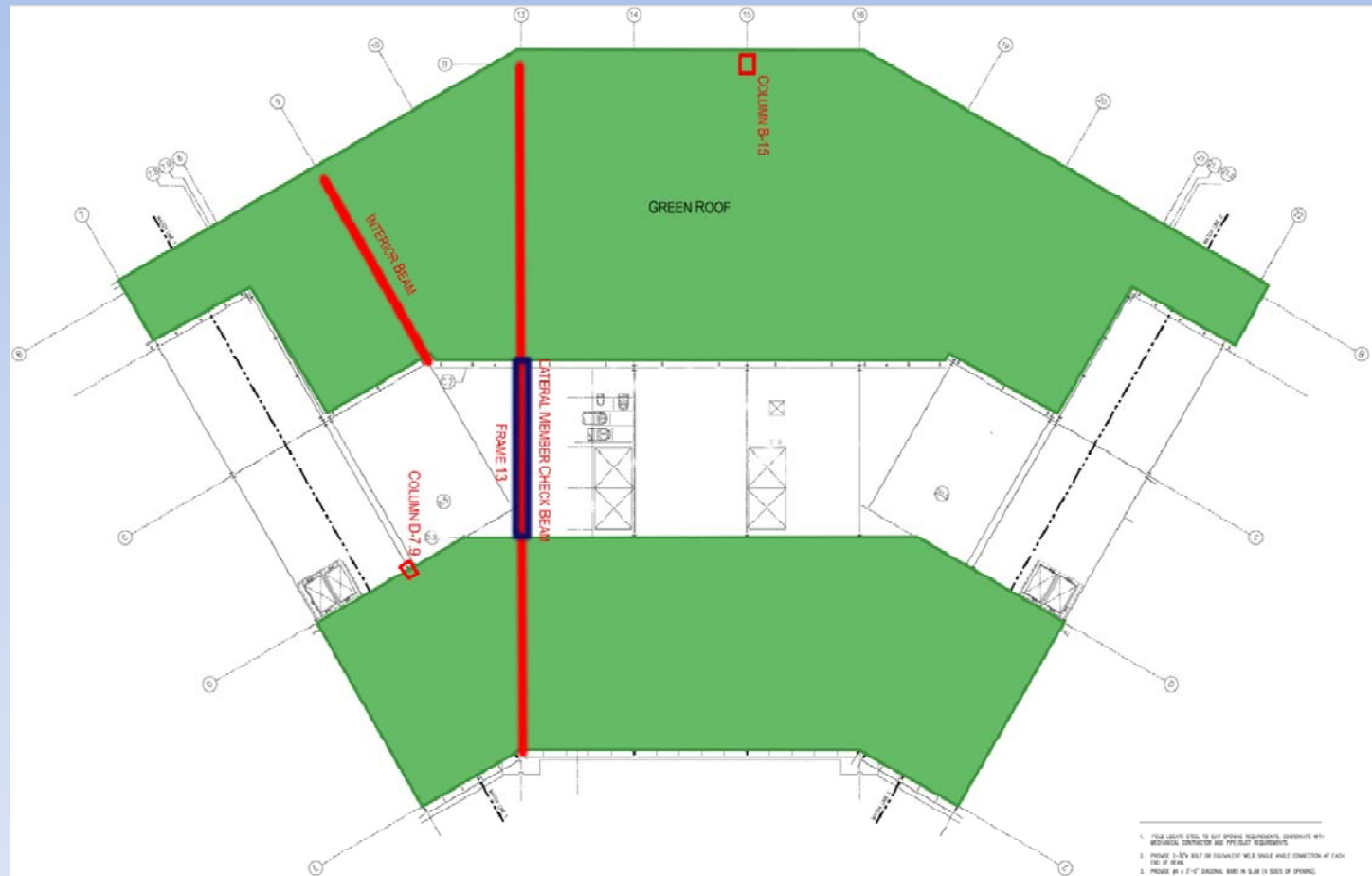
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## ROOF CENTER



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Whole Building Steel



West Building Steel



East Building Steel

Pictures taken by Jessica L. Laurito on 8/19/2008

# REFERENCE SLIDE

## PORTAL METHOD ANALYSIS FOR REDESIGNED

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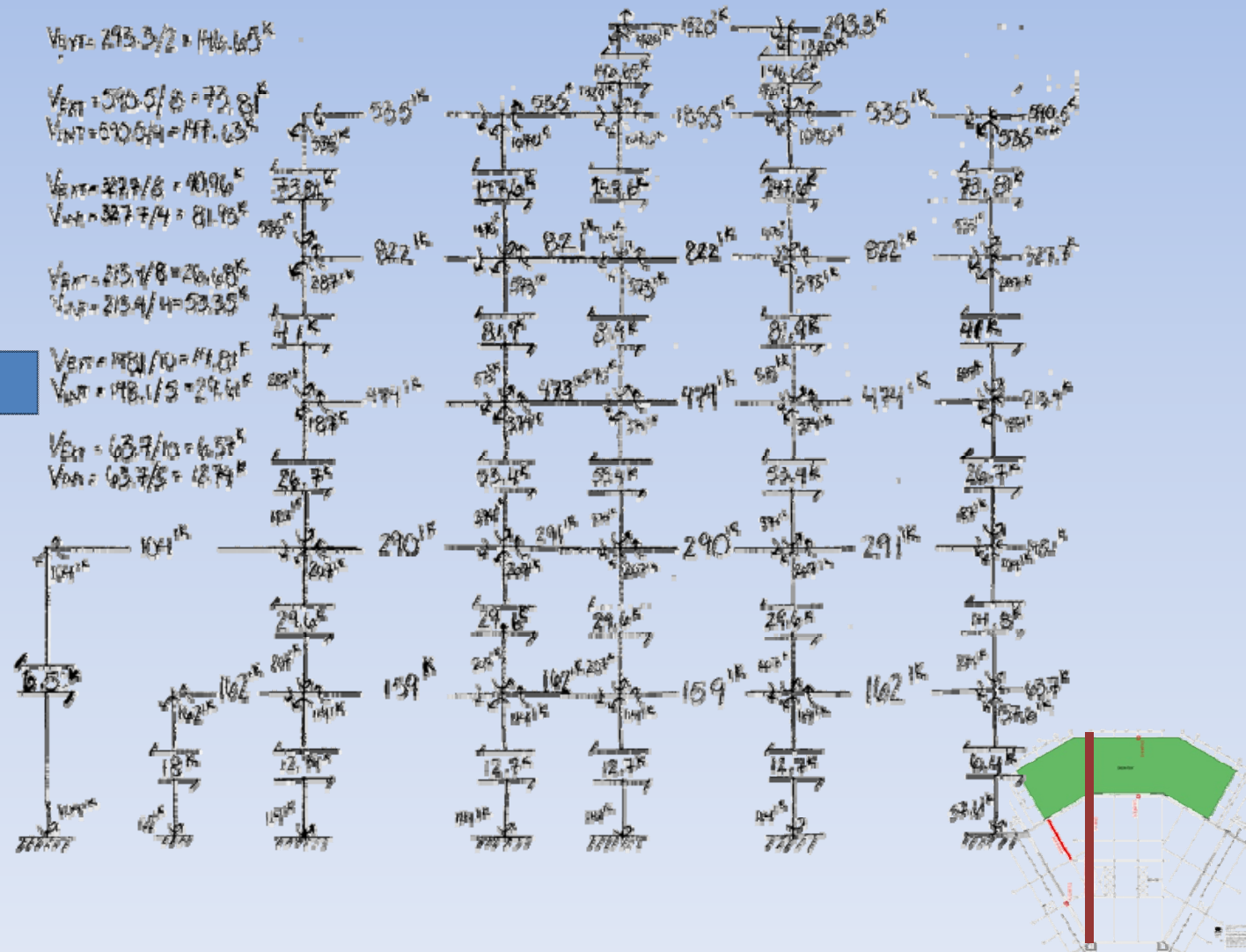
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## HAND CALCULATED BEAM

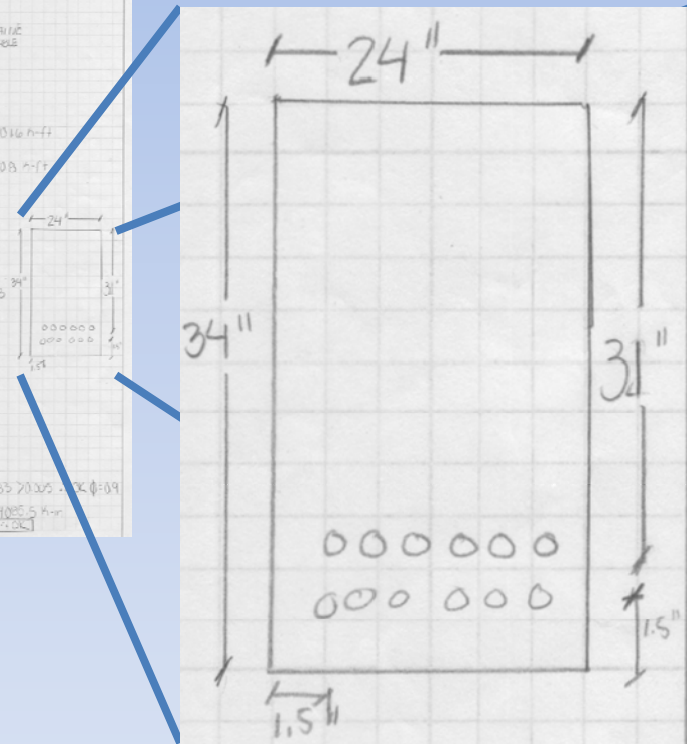
### Preliminary Beam Design

**GRABER DESIGN - INTERIOR - FLOOR**  
 LAYOUT: 20'0" PSF + 10'0" PSF + GRABER WT  
 LIVE: 20'0" PSF + 10'0" PSF

9" NO LIVE LOAD REDUCTION TO BE CONSIDERED  
 SINCE TYPICAL FIN-FLOOR DUCTS UNAVAILABLE  
 WLL =  $1.2(20+10) + 1.6(20+20) = 272$  PSF  
WLL = 272 PSF

**MAXIMUM MOMENT DETERMINATION**  
 $M_{max @ 0.405} = \frac{wL^2}{12} = \frac{(0.272 \text{ ksf})(24 \times 12)^2}{12} = 10316 \text{ ft-lb}$   
 $M_{max @ 1.0} = \frac{wL^2}{24} = \frac{(0.272 \text{ ksf})(24 \times 12)^2}{24} = 5508 \text{ ft-lb}$

**GRABER SIZE**  
 $W_d = 20 \text{ kips}$   
 $2d = 20 \text{ (102)} = 20 \text{ (102)}$   
 $d = 20 \text{ (102)}$   
 $n = 2 + 15 + 0.6/2 = 20.3 + 0.3 = 20.6$   
 $[f = 91] \quad d = 11.5 \times 20.6 = 237 \text{ (118)}$   
 $A_s = \frac{M_u}{f_y} = \frac{10316}{80000} = 0.129 \text{ in}^2$   
 TRY 12" #3 @ 2 EQUALS,  $A_s = 0.148 \text{ in}^2$   
 Assume  $f_s = f_y$   
 $c = \frac{f_y}{f_c} = \frac{80000}{4000} = 20$   
 $d = \frac{f_y}{f_c} = \frac{80000}{4000} = 20$   
 CHECK  $f_s > f_y$   
 $f_s = \frac{M_u}{A_s d} = \frac{10316}{0.148 \times 20} = 3460 \text{ psi} < 4000 \text{ psi}$   
 $\phi M_n = \phi [A_s f_y (d - c)] = 0.9 [0.148 \times 80000 (20 - 2)] = 20055 \text{ ft-lb}$   
 $\phi M_n = 1175 \text{ (58)} > 1116 \text{ (54)} \text{ OK}$



**MINIMUM SHEAR REINF.**  
 $v_u = \text{Max} \left\{ \frac{0.15 \sqrt{f_c} w_u}{f_y}, \frac{0.75 \sqrt{f_c} w_u}{f_y} \right\} = \frac{0.75 \sqrt{4000} (24 \times 12 \times 1000)}{80000} = 0.289 \text{ ksi}$   
 $v_u = 0.289 \text{ ksi}$   
 $A_v = \frac{v_u b d}{f_y} = \frac{0.289 \times 24 \times 12 \times 1000}{80000} = 0.108 \text{ in}^2$   
 #3 STEEL @ 15" AS MINIMUM SHEAR REINF.  
 $(2 \text{ LEGS} = 2 \times 0.11 \text{ in}^2) = 0.22 \text{ in}^2 > 0.108 \text{ in}^2 \text{ OK}$

**SHEAR REINF.**  
 $v_u = \frac{V_u}{b d} = \frac{10316}{24 \times 12 \times 1000} = 0.357 \text{ ksi}$   
 $v_u = 0.357 \text{ ksi}$   
 $A_v = \frac{v_u b d}{f_y} = \frac{0.357 \times 24 \times 12 \times 1000}{80000} = 0.131 \text{ in}^2$   
 #3 @ 12" @ 12" WORKS  
 $v_u = \frac{V_u}{b d} = \frac{10316}{24 \times 12 \times 1000} = 0.357 \text{ ksi}$   
 WHERE WHERE  $v_u > 0.357 \text{ ksi}$   
 $v_u = \frac{1.1 \times 10316}{24 \times 12 \times 1000} = 0.375 \text{ ksi}$   
 $v_u = 0.375 \text{ ksi}$

17.5" - 12" - 110" - 12" - 77.5"  
 2005 - 1000 - NO STIRR REQUIRED - 1000 - 2005

Based on this preliminary design and interior gravity beam can be 24"x34"

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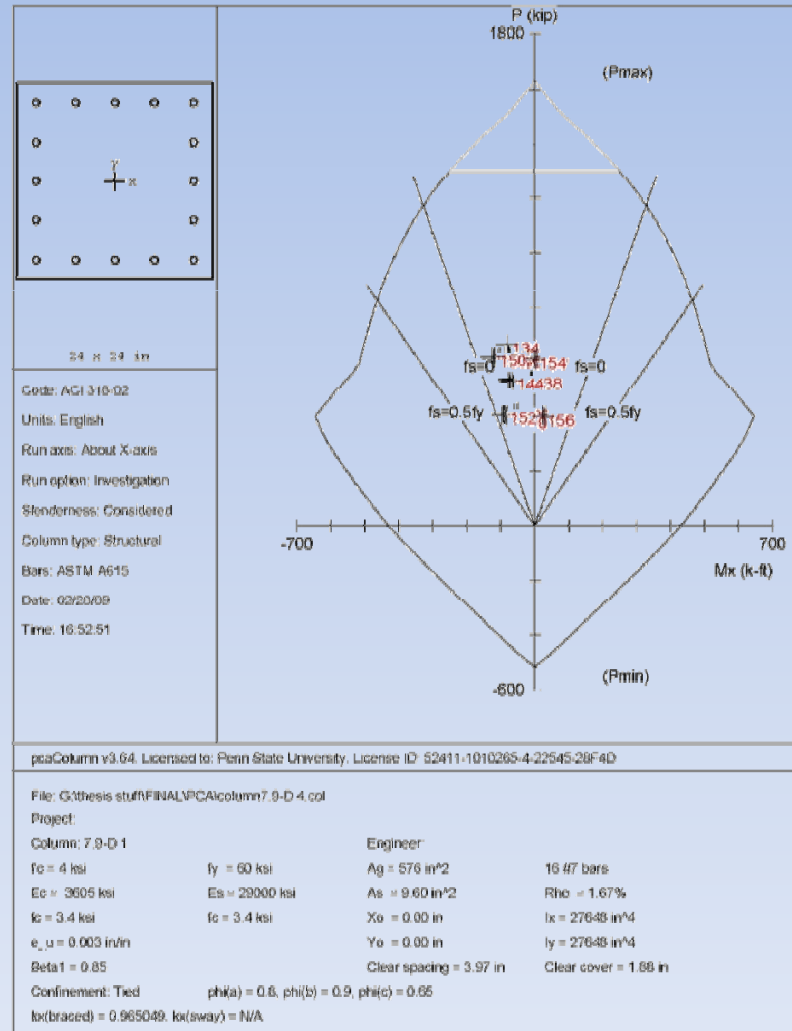
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## PCA COLUMN CHECK Column D-7.9 Fourth Floor



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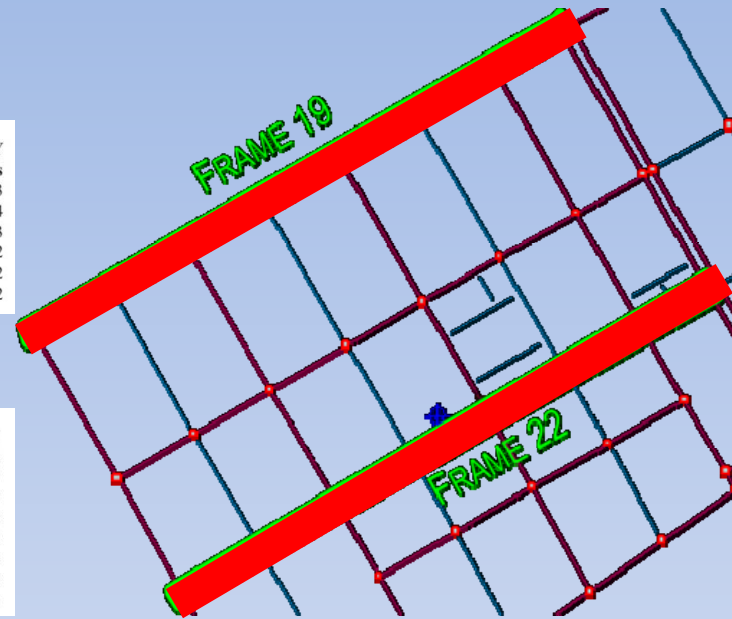
Acknowledgements

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## Wind Frame 19

Level	Wind Shear-X kips	Wind Change-X kips	Wind Shear-Y kips	Wind Change-Y kips
Roof	24.27	24.27	17.43	17.43
Fifth	29.05	4.78	20.97	3.54
Fourth	43.42	14.37	31.90	10.93
Third	51.17	7.75	38.22	6.32
Second	46.66	-4.51	33.40	-4.82
First	-9.04	-55.70	-11.12	-44.52

## TORSION



## Wind Frame 22

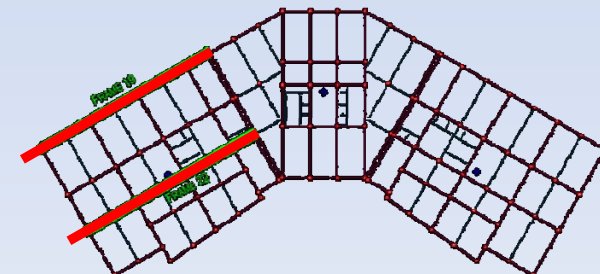
Level	Wind Shear-X kips	Wind Change-X kips	Wind Shear-Y kips	Wind Change-Y kips
Penthouse	3.26	3.26	3.47	3.47
Roof	3.71	0.45	7.56	4.10
Fifth	9.77	6.06	15.69	8.12
Fourth	12.68	2.91	20.61	4.92
Third	18.67	5.99	27.52	6.92
Second	19.37	0.70	35.57	8.05
First	-3.24	-22.62	-10.30	-45.87

## Seismic Frame 19

Level	Seismic Shear-X kips	Seismic Change-X kips	Seismic Shear-Y kips	Seismic Change-Y kips
Roof	50.00	50.00	15.85	15.85
Fifth	49.63	-0.37	14.53	-1.33
Fourth	64.72	15.09	19.06	4.54
Third	66.40	1.68	20.10	1.04
Second	73.12	6.72	15.00	-5.10
First	23.19	-96.31	7.26	-7.74

## Seismic Frame 22

Level	Seismic Shear-X kips	Seismic Change-X kips	Seismic Shear-Y kips	Seismic Change-Y kips
Penthouse	20.03	20.03	6.15	6.15
Roof	26.35	6.32	-6.05	-12.20
Fifth	47.99	21.64	-4.00	2.05
Fourth	56.10	8.12	-5.38	-1.38
Third	65.66	9.56	-5.03	0.35
Second	60.39	-5.28	-4.42	0.61
First	-17.19	-77.57	6.33	10.75



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## DRIFT FOR REDESIGNED BUILDING

		Controlling Seismic						
Story	St heig	Story	Story height (ft)	Actual Drift Ratio	Allowable $\delta_{xe}/h_{sx}=0.02*1.0/3$	Total Drift Ratio	ble Total Drift (in)	
							$\Delta_{Wind}=H/400$	
Pent		Pent	92.5	0.0004	<	0.006667	75	Acceptable
Roof		Roof	74.5	0.0005	<	0.006667	85	Acceptable
5		5	60.0	0.0008	<	0.006667		Acceptable
4		4	46.0	0.0009	<	0.006667	8	Acceptable
3		3	32.0	0.001	<	0.006667	6	Acceptable
2		2	18.0	0.0009	<	0.006667	4	Acceptable

## DRIFT FOR THE AS-BUILT STEEL BUILDING

		Controlling Wind					
Story	Story height (ft)	Story Drift (in)	Allowable Story Drift (in) $\Delta_{Wind}=H/400$		Total Drift (in)	Allowable Total Drift (in) $\Delta_{Wind}=H/400$	
Roof	74.5	0.127	< 0.435	Acceptable	1.02425	< 2.235	Acceptable
5	60.0	0.187	< 0.42	Acceptable	0.89767	< 1.8	Acceptable
4	46.0	0.247	< 0.42	Acceptable	0.71044	< 1.38	Acceptable
3	32.0	0.257	< 0.42	Acceptable	0.46336	< 0.96	Acceptable
2	18.0	0.207	< 0.54	Acceptable	0.20662	< 0.54	Acceptable

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## SEISMIC CALCULATIONS

### Redesigned Values

Seismic Design Values, ASCE 7-05		
Response Modification Coefficient	R= 3	Table 12.2-1
Coefficient	$C_U= 1.7$	Table 12.8-1
Fundamental Period	T= 1.5999	Sec. 12.8.2
Seismic Response Coefficient	$C_S= 0.015$	Eq. 12.8-3
Building Height (above grade)	h= 92.5	

### As-Built Values

Seismic Design Values, ASCE 7-05			
Response Modification Coefficient	R= 3	R= 3.5	Table 12.2-1
Coefficient	$C_U= 1.7$	$C_U= 1.7$	Table 12.8-1
Fundamental Period	T= 1.780	T= 1.780	Sec. 12.8.2
Seismic Response Coefficient	$C_S= 0.014$	$C_S= 0.012$	Eq. 12.8-3
Building Height (above grade)	h= 92.5	h= 92.5	



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Seismic Design Values, ASCE 7-05

Occupancy	II	Table 1-1
Importance Factor	I= 1	Table 11.5-1
Site Class	D	Table 20.3-1
Spectral Response Acceleration, short	$S_S = 0.12$	Figure 22-1
Spectral Response Acceleration, 1 sec	$S_1 = 0.046$	Figure 22-2
Site Coefficient $F_a$	$F_a = 1.6$	Table 11.4-1
Site Coefficient $F_v$	$F_v = 2.4$	Table 11.4-2
MCE Spectral Response Acceleration, short	$S_{MS} = 0.192$	Eq. 11.4-1
MCE Spectral Response Acceleration, 1 sec	$S_{M1} = 0.1104$	Eq. 11.4-2
Design Spectral Acceleration, short	$S_{DS} = 0.128$	Eq. 11.4-3
Design Spectral Acceleration, 1 sec	$S_{D1} = 0.0736$	Eq. 11.4-4
Seismic Design Category	B	Table 11.6-1

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## SEISMIC CALCULATIONS

Calculated Values		USGS Website Values
$S_S = 0.12$	(From Figure 22-1)	$S_S = 0.125$
$S_1 = 0.046$	(From Figure 22-2)	$S_1 = 0.048$
$S_{MS} = F_a * S_S = 0.192$		$S_{MS} = 0.2$
$S_{M1} = F_V * S_1 = 0.1104$		$S_{M1} = 0.116$
$S_{DS} = 2S_{MS}/3 = 0.128$	A (Table 11.6-1)	$S_{DS} = 0.133$
$S_{D1} = 2S_{M1}/3 = 0.0736$	B (Table 11.6-2)	$S_{D1} = 0.077$

$F_a$ Values (Table 11.4-1 ASCE 7-05)					
	$S_S \leq 0.25$	$S_S = 0.5$	$S_S = 0.75$	$S_S = 1.0$	$S_S \geq 1.25$
D	1.6	1.4	1.2	1.2	1

$F_V$ Values (Table 11.4-2 ASCE 7-05)					
	$S_1 \leq 0.1$	$S_1 = 0.3$	$S_1 = 0.3$	$S_1 = 0.4$	$S_1 \geq 0.5$
D	2.4	2	1.8	1.6	1.5

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## SEISMIC CALCULATIONS

### Redesigned Values

$$C_T = 0.016 \quad (\text{From Table 12.8-2})$$

$$X = 0.9 \quad (\text{From Table 12.8-2})$$

$$T_a = C_t h_n^x = 0.9411255$$

$$T_s = S_{D1}/S_{DS} = 0.575$$

$$0.8T_s = 0.46 < T_a \text{ therefore must use Table 11.6-1,2}$$

$$T_L = 12 \quad (\text{From Fig. 22-15 p. 228 ASCE 7-05})$$

$$C_s = \text{MAX}$$

$$\text{for } T > T_L$$

$$S_{DS}/(R/I) = 0.0427 \quad (12.8-2)$$

$$S_{D1}/(T^*R/I) = 0.0153 \quad (12.8-3)$$

$$S_{D1}T_L/(T^2R/I) = 0.3324 \quad (12.8-4)$$

$$\geq 0.01 \quad (12.8-5)$$

$$C_s = 0.0153$$

$$T = C_U * T_a = 1.5999134$$

$$V = C_s * W = 1636.69$$

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## WIND CALCULATIONS

Basic Wind Speed (V) mph	90
Exposure Category	B
Importance Factor (I)	1
Wind Directionality Factor (Kd)	0.85
Topographic Factor (Kzt)	1

From Table 6-3

H (ft)	K <sub>z</sub>	q <sub>z</sub>
92.5	0.9675	14.354
74.5	0.908	13.471
60	0.85	12.611
46	0.79	11.720
32	0.712	10.563
18	0.59	8.902
0	0.57	8.456

From RAM

H (ft)	K <sub>z</sub>	q <sub>z</sub>
92.5	0.966	14.331
74.5	0.909	13.486
60	0.854	12.670
46	0.792	11.750
32	0.714	10.593
18	0.605	8.976
0	0.575	8.531

Floor Heights	Level	Total Height	K <sub>z</sub>	q <sub>z</sub>	Wind Pressures (psf)					
					N-S Windward	N-S Leeward	N-S Side Wall	E-W Windward	E-W Leeward	E-W Sidewall
18	Penthouse	92.5	0.9675	14.354	11.54	-8.21	-10.43	12.20	-4.91	-10.49
14.5	Roof	74.5	0.908	13.471	10.99	-8.21	-10.43	11.61	-4.91	-10.49
14	5	60	0.85	12.611	10.46	-8.21	-10.43	11.43	-4.91	-10.49
14	4	46	0.79	11.720	9.91	-8.21	-10.43	11.04	-4.91	-10.49
14	3	32	0.712	10.563	9.20	-8.21	-10.43	10.65	-4.91	-10.49
18	2	18	0.59	8.902	7.90	-8.21	-10.43	10.45	-4.91	-10.49

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## WIND CALCULATIONS

Level	Wind Design					
	Load (kips)		Shear (kips)		Moment (ft-k)	
	N-S	E-W	N-S	E-W	N-S	E-W
Pent	193.4	38.8	0	0	3481.3	698.2
Roof	151.5	30.2	193.4	38.8	2196.7	437.6
5	144.8	29.3	344.9	69.0	2026.7	410.7
4	138.0	28.1	489.7	98.3	1932.5	393.8
3	132.6	27.4	627.7	126.4	1856.3	384.1
2	140.2	31.0	760.3	153.9	2523.7	557.2
Total	900.5	184.8	900.5	184.8	10535.9	2183.4

Level	Wind Design					
	Load (kips)		Shear (kips)		Moment (ft-k)	
	N-S	E-W	N-S	E-W	N-S	E-W
Roof	151.6	30.5	0	0	2198.6	442.4
5	144.8	29.7	151.6	30.5	2026.7	415.2
4	137.9	28.4	296.4	60.2	1930.7	397.7
3	132.3	27.7	434.3	88.6	1852.1	387.5
2	139.5	31.2	566.6	116.3	2511.1	562.0
Total	706.1	147.5	706.1	147.5	10519.2	2204.8

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## WIND CALCULATIONS

$$q_p = 0.00256 K_r K_{zt} K_d V^2 I = 14.836$$

$$GC_{pn} = 1.5 \quad -1$$

$$P_p = q_p GC_{pn} = 22.254 \quad -14.836$$

Basic Wind Speed (V) mph	90
Exposure Category	B
Importance Factor (I)	1
Wind Directionality Factor (K <sub>d</sub> )	0.85
Topographic Factor (K <sub>zt</sub> )	1

$$n_1 = \frac{43.5}{H^{0.9}} = 1.163 \text{ eq (C6-15)} \quad n_1 > 1 \quad \text{therefore Rigid structure}$$

$$g_Q = g_V = 3.4$$

$$G = 0.85$$

$$z = 0.6h = 55.5$$

$$z_{min} = 30'$$

$$I_z = c(33/z)^{1/6} = 0.275$$

$$L_z = I(z/33)^6 = 380.55$$

$$Q_{N-S} = \sqrt{1/(1+0.63(B+h/L_z)^{0.63})} = 0.731$$

$$Q_{E-W} = \sqrt{1/(1+0.63(B+h/L_z)^{0.63})} = 0.832$$

$$G_{fN-S} = 0.925 [(1+1.7I_z g_Q Q)/(1+1.7g_V I_z)] = 0.7722744$$

$$G_{fE-W} = 0.925 [(1+1.7I_z g_Q Q)/(1+1.7g_V I_z)] = 0.8296736$$

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## FOUNDATION IMPLICATIONS

### Caissons

#### Uncored Caisson

Axial capacity = area x allow bearing - weight of caisson

Uplift capacity NON-EMBEDDED CAISSON = Soli Friction + Weight of Caisson

0 ft Embedment					CAISSON	
Pile D [ft]	Area [sf]	Circumf. [ft]	Weight [kips]	Tu [kips] w/ SF	Uplift Capacity w/o Core [kips]	Axial Capacity w/o Core [kips]
<u>5.00</u>	19.63	15.71	35.83	12.04	47.87	553.21
<u>5.50</u>	23.76	17.28	43.36	13.24	56.60	669.39
<u>6.00</u>	28.27	18.85	51.60	14.44	66.04	796.63
<u>6.50</u>	33.18	20.42	60.56	15.65	76.21	934.93
<u>7.00</u>	38.48	21.99	70.23	16.85	87.08	1084.30
<u>7.50</u>	44.18	23.56	80.63	18.05	98.68	1244.73
Length = 12.17 ft						

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## FOUNDATION IMPLICATIONS

### Spread footings

soil bearing      8 ksf  
caisson bearing    30 ksf

$$q_u = P_u / A$$

$$d^2(4VC+q)+d(2VC+q)w=q(BL-w)$$

#### Punching Shear

$$V_c \leq \phi(2+4\beta_c)\sqrt{f_c}b_o d$$

$$\phi 4\sqrt{f_c}b_o d$$

$$\phi(\alpha_s d/b_o + 2)\sqrt{f_c}b_o d$$

$$\phi = 0.75$$

$$\beta_c = 1$$

$$f_c = 3000$$

$$\alpha = 40$$

int

$$30$$

edge

$$20$$

corner